# METR4202 -- Robotics Tutorial 5 – Week 5: Trajectory Generation & Motion Planning

#### Reading

Please read/review chapter 9 of Robotics, Vision and Control.

### Questions

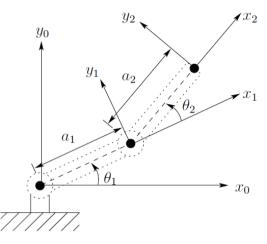


Figure 1: Two DOF Robot manipulator

1. Write the full equation of motion for the 2R arm above (i.e.,  $\tau_1$  and  $\tau_2$  as a function of  $\theta_1$  and  $\theta_2$  and its derivatives)

### Start with the masses of links: $m_1$ and $m_2$ , to get the Mass Matrix recall (lecture 5)

$$M = \sum_{i=1}^{N} \left( m_{i} J_{\nu_{i}}^{T} J_{\nu_{i}} + J_{\omega_{i}}^{T} I_{C_{i}} J_{\omega_{i}} \right)$$
  
$$M = m_{1} J_{\nu_{1}}^{T} J_{\nu_{1}} + J_{\omega_{1}}^{T} I_{1} J_{\omega_{1}} + m_{2} J_{\nu_{2}}^{T} J_{\nu_{2}} + J_{\omega_{2}}^{T} I_{2} J_{\omega_{2}}$$

Note that:  $m_i$  = the mass of the i<sup>th</sup> link  $m_{ii}$  = the ij element of the mass matrix

$$m_{ijk} \equiv \frac{\partial m_{ij}}{\partial q_k}$$

Note this is with respect to the configuration variable, not time.

On that subject, the derivative with respect to time would be:  $\frac{d}{dt}m_{ij} = \sum_{k=1}^{N} m_{ijk}\dot{q}_k$ 

The center of mass of each link is at the joint center, this  $l_1 \equiv a_1/2$  and  $l_2 \equiv a_2/2$ 

To compute the Jacobians ( $J_v$  and  $J_\omega$ ), we need to calculate the forward kinematics.

Recall that the position vectors (Lec 3, Slide 34) for a 2R arm are:

$${}^{0}P_{1} = \begin{bmatrix} a_{1}C_{1} \\ a_{1}S_{1} \\ 0 \end{bmatrix}$$
 (this reads as "Position of Frame 1 as seen in 0"),  ${}^{0}P_{2} = \begin{bmatrix} a_{1}C_{1} + a_{2}C_{12} \\ a_{1}S_{2} + a_{2}S_{12} \\ 0 \end{bmatrix}$ 

Thus with respect to Frame {0}, the translational velocity Jacobians (i.e., the matrices that encode the differential relationship between joint velocities and workspace tip velocities) are found by direct differentiation of the position vectors  ${}^{0}\mathbf{P}_{1}$  and  ${}^{0}\mathbf{P}_{2}$ .

$${}^{0}J_{v_{1}} = \begin{bmatrix} -a_{1}S_{1} & 0 \\ a_{1}C_{1} & 0 \\ 0 & 0 \end{bmatrix}, {}^{0}J_{v_{2}} = \begin{bmatrix} -a_{1}S_{1} - a_{1}S_{12} & -a_{2}S_{12} \\ a_{1}C_{1} + a_{2}C_{12} & a_{2}C_{12} \\ 0 & 0 \end{bmatrix}$$
$$\rightarrow m_{1}J_{v_{1}}^{T}J_{v_{1}} = \begin{bmatrix} m_{1}a_{1}^{2} & 0 \\ 0 & 0 \end{bmatrix}, m_{2}J_{v_{2}}^{T}J_{v_{2}} = \begin{bmatrix} m_{2}\left(a_{1}^{2} + a_{2}^{2} + 2a_{1}a_{2}C_{2}\right) & m_{2}\left(a_{2}^{2} + a_{1}a_{2}C_{2}\right) \\ m_{2}\left(a_{2}^{2} + a_{1}a_{2}C_{2}\right) & m_{2}a_{2}^{2} \end{bmatrix}$$

The rotational velocity Jacobian matrices with respect to Frame {0} are given by  $J_{\omega_1} = \begin{bmatrix} \overline{\varepsilon}_1 \mathbf{z}_1 & \mathbf{0} \end{bmatrix}, J_{\omega_2} = \begin{bmatrix} \overline{\varepsilon}_1 \mathbf{z}_1 & \overline{\varepsilon}_2 \mathbf{z}_2 \end{bmatrix}$ 

As both joints are revolute ( $\varepsilon$ =0), these matrices are  $J_{\omega_1} = \begin{bmatrix} \mathbf{z}_1 & \mathbf{0} \end{bmatrix}, J_{\omega_2} = \begin{bmatrix} \mathbf{z}_1 & \mathbf{z}_2 \end{bmatrix}$ 

Thus,  $J_{\omega_1} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1 & 0 \end{bmatrix}, J_{\omega_2} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1 & 1 \end{bmatrix}$ , and after some substitution and simplification we have

$$J_{\omega_1}^T I_1 J_{\omega_1} = \begin{bmatrix} I_1 & 0 \\ 0 & 0 \end{bmatrix}, J_{\omega_2}^T I_2 J_{\omega_2} = \begin{bmatrix} I_2 & I_2 \\ I_2 & I_2 \end{bmatrix} \text{ where I is about the z-axis } (I_1 = I_{\{zz\}1} \text{ and } I_2 = I_{\{zz\}2})$$
  
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$$M = \begin{bmatrix} m_1 a_1^2 + I_1 + m_2 \left( a_1^2 + a_2^2 + 2a_1 a_2 C_2 \right) + I_2 & m_2 \left( a_2^2 + a_1 a_2 C_2 \right) + I_2 \\ m_2 \left( a_2^2 + a_1 a_2 C_2 \right) + I_2 & m_2 a_2^2 + I_2 \end{bmatrix}$$

The Centrifugal and Coriolis Matrix  $\mathbf{v}$  is found directly by recalling Christoffel symbols (please review Christoffel symbols from dynamics and the mass notation from the previous page)

$$b_{i,jk} = \frac{1}{2} \left( m_{ijk} + m_{ikj} - m_{jki} \right)$$
 and with  $b_{iii} = b_{iji} = 0$ ,

the Centrifugal matrix becomes

$$B = \begin{bmatrix} 2b_{112} \\ 0 \end{bmatrix} = \begin{bmatrix} \frac{1}{2}m_{112} \\ 0 \end{bmatrix} = \begin{bmatrix} \frac{1}{2}\left(\frac{\partial m_{11}}{\partial \partial_2}\right) \\ 0 \end{bmatrix} = \begin{bmatrix} -m_2a_1a_2S_2 \\ 0 \end{bmatrix}$$

and the Coriolis matrix can be written as

$$C = \begin{bmatrix} 0 & b_{122} \\ b_{211} & 0 \end{bmatrix} = \begin{bmatrix} 0 & m_{122} \\ -\frac{1}{2}m_{112} & 0 \end{bmatrix} = \begin{bmatrix} 0 & \left(\frac{\partial m_{12}}{\partial \partial_2}\right) \\ -\frac{1}{2}\left(\frac{\partial m_{11}}{\partial \partial_2}\right) & 0 \end{bmatrix} = \begin{bmatrix} 0 & -m_2 a_1 a_2 S_2 \\ m_2 a_1 a_2 S_2 & 0 \end{bmatrix}$$

Summing this together gives

$$V = \begin{bmatrix} -m_2 a_1 a_2 S_2 \\ 0 \end{bmatrix} (\dot{\theta}_1 \dot{\theta}_2) + \begin{bmatrix} 0 & -m_2 a_1 a_2 S_2 \\ m_2 a_1 a_2 S_2 & 0 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1^2 \\ \dot{\theta}_2^2 \end{bmatrix}$$

The next factor to consider is gravity.

While the problem does not specify a gravity direction, we assume it is acting parallel to the y-axis. This gives  $\mathbf{g} = \begin{bmatrix} 0 & -g & 0 \end{bmatrix}$ . (Note that if we latter wish to assume that gravity is acting along the *z*-axis (into the page), this could be treated by setting  $\mathbf{g} = \begin{bmatrix} 0 & 0 & -g \end{bmatrix}$ )

With respect to Frame  $\{0\}$ , the gravity vector can be calculated as

$$\mathbf{G} = -\left[J_{v_{C1}}^T m_{C1}\mathbf{g} + J_{v_{C2}}^T m_{C2}\mathbf{g}\right]$$

However, we have to be careful because the gravity acts at the mass center (which is represented by the notation C1 and C2). Again, recall that we have  $l_1=a_1/2$  and  $l_2=a_2/2$  Given the structure of the problem, the Jacobbians are be determined by inspection. Thus,

$${}^{0}G = -\begin{bmatrix} -l_{1}S_{1} & l_{1}C_{1} & 0\\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0\\ -m_{1}g\\ 0 \end{bmatrix} - \begin{bmatrix} -a_{1}S_{1} - l_{2}S_{12} & a_{1}C_{1} + l_{2}C_{12} & 0\\ -l_{2}S_{12} & l_{2}C_{12} & 0 \end{bmatrix} \begin{bmatrix} 0\\ -m_{2}g\\ 0 \end{bmatrix}$$
$${}^{0}G = \begin{bmatrix} (m_{1}l_{1} + m_{2}a_{1})C_{1} + m_{2}l_{2}C_{12}\\ m_{2}l_{2}C_{12} \end{bmatrix} (g) = \begin{bmatrix} (\frac{1}{2}m_{1} + m_{2})a_{1}C_{1} + \frac{1}{2}m_{2}a_{2}C_{12}\\ \frac{1}{2}m_{2}a_{2}C_{12} \end{bmatrix} (g)$$

The **Equations of Motion** can be found by putting these terms together to give (for review see also Lecture 4, Slide 30 and Lecture 5, Slide 7)

$$\begin{aligned} \mathbf{\tau} &= M\left(\theta\right)\ddot{\mathbf{\theta}} + \mathbf{v}\left(\mathbf{\theta},\dot{\mathbf{\theta}}\right) + \mathbf{g}\left(\mathbf{\theta}\right) \\ \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} &= \begin{bmatrix} m_1a_1^2 + I_1 + m_2\left(a_1^2 + a_2^2 + 2a_1a_2C_2\right) + I_2 & m_2\left(a_2^2 + a_1a_2C_2\right) + I_2 \\ m_2\left(a_2^2 + a_1a_2C_2\right) + I_2 & m_2a_2^2 + I_2 \end{bmatrix} \begin{bmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{bmatrix} \\ &+ \left(\dot{\theta}_1\dot{\theta}_2\right) \begin{bmatrix} -m_2a_1a_2S_2 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 & -m_2a_1a_2S_2 \\ m_2a_1a_2S_2 & 0 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1^2 \\ \dot{\theta}_2^2 \end{bmatrix} + \left(g\right) \begin{bmatrix} \left(\frac{1}{2}m_1 + m_2\right)a_1C_1 + \frac{1}{2}m_2a_2C_{12} \\ \frac{1}{2}m_2a_2C_{12} \end{bmatrix} \end{aligned}$$

## **Challenge Question:**

Inverse Kinematics & Trajectory Generation

A small humanoid robot is being programmed to place a hat on its head. The objective is to place the hat in the position shown by the dashed outline in the figure below. Assume that the arm is composed of 3 revolute joints and is constrained to move in the plane of the page. The arm consists of 3 links with dimensions:  $L_1=0.4$ ,  $L_2=0.3$ ,  $L_3=0.1$ .

In order to place the hat on its head, assume that we must place the edge of the hat brim at a location 0.5m above its shoulder joint. The hat brim should be in a horizontal position and is gripped at its edge by the hand and is aligned with the last link of the arm. Please calculate/plot valid workspace (e.g., from the frame located at the right-most end of the brim where the robot is grasping it) and joint trajectories to place the hat correctly.

