The University Of Queensland

AUSTRALIA

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# School of Information Technology and Electrical Engineering EXAMINATION 

Semester One Final Examinations, 2013

## ELEC3004 Signals, Systems \& Control

This paper is for St Lucia Campus students.
Examination Duration:
Reading Time:
Exam Conditions:
This is a Central Examination

This is a Closed Book Examination - specified materials permitted
During reading time - write only on the rough paper provided
This examination paper will be released to the Library

## Materials Permitted In The Exam Venue:

(No electronic aids are permitted e.g. laptops, phones)
Any unmarked paper dictionary is permitted
An unmarked Bilingual dictionary is permitted
Calculators - Any calculator permitted - unrestricted
One A4 sheet of handwritten or typed notes double sided is permitted

## Materials To Be Supplied To Students:

$1 \times 14$ Page Answer Booklet
$1 \times 1 \mathrm{~cm} \times 1 \mathrm{~cm}$ Graph Paper
Rough Paper
Instructions To Students:
Please answer ALL questions. Thank you.

This exam has THREE (3) Sections for a total of 100 Points
Section 1: Linear Systems ..... 30 \%
Section 2: Signal Processing ..... 30 \%
Section 3: Digital Control ..... 40 \%
Please answer ALL questions
Section 1: Linear Systems
Please Record Answers in the Answer Book

## 1. Convolution

Determine the continuous time convolution of $\mathbf{x}(\mathbf{t})$ and $\mathbf{h}(\mathbf{t})$. Assume that they are both of the same unity amplitude.


## 2. Does Linearity Imply Invertibility?

IF $\mathbf{F}$ is a linear, time-invariant system such that $\mathrm{y}=\mathbf{F}[\mathrm{x}]$,
THEN is there another Linear System (G) for which $\mathrm{x}=\mathbf{G}[\mathrm{y}]$ ?

## 3. Causality and Stability

A continuous-time LTI system has impulse response function

$$
h(t)=\sum_{i=0}^{\infty}(0.5)^{i} \delta(t-i)
$$

Is the system, $\mathrm{h}(\mathrm{t})$, causal? Is it BIBO stable? (Please briefly justify)

## 4. Linearity Ahoy!

Dr Shilling pensively does tests on a new system $\mathbf{F}$ with inputs $\boldsymbol{x}[\boldsymbol{n}]$ to get outputs $\boldsymbol{y}[\boldsymbol{n}]$ and observes the following input/output signal pairs (for $n=1$ to 5 ):

| $\boldsymbol{i}$ | Input $\left(\boldsymbol{x}_{i}[\mathbf{n}]\right)$ | Output $\left(\boldsymbol{y}_{\mathbf{i}}[\mathbf{n}]\right)$ |
| :---: | :---: | :---: |
| 1 | $[0,0,0,1,1]$ | $[0,1,0,0,0]$ |
| 2 | $[0,1,1,1,1]$ | $[0,1,0,1,0]$ |
| 3 | $[0,1,1,2,2]$ | $[0,2,0,1,0]$ |

(In all cases below please briefly justify your answers)
a) From this, can $\operatorname{Dr}$ Shilling conclude that the system $\mathbf{F}$ is linear?
b) Assume that $\mathbf{F}$ is indeed linear, then is it possible to determine the output signal associated with an input of $\boldsymbol{x}=[0,0,0,0,0]$ ? If so, please compute it.
c) Assume that $\mathbf{F}$ is indeed linear, then is it possible to determine the input signal associated with an output of $\mathbf{y}=[0,0,0,0,0]$ ? If so, please compute it.
5. Characteristic Roots and Characteristic Modes

For systems having the following pole-zero plots (on the complex plane), please sketch the corresponding zero-input response.


## 6. Second Order Systems

Consider the following series RLC circuit system.

Recall that for such a circuit, the response is second order and that $\omega_{0}=\frac{1}{\sqrt{L C}}, \alpha=\frac{R}{2 L}$ and $\zeta=\frac{\alpha}{\omega_{0}}$


Determine the $\mathbf{C}$ for a circuit with $\mathrm{R}=1 \Omega, \mathrm{~L}=4 \mathrm{H}$ and the following impulse response: (hint: the values might be larger than "common" parts)


## Section 2: Signal Processing

Please Record Answers in the Answer Book

## 7. What a Difference

Does the difference equation

$$
y[k]+k^{2} y[k-1]-2 y[k-2]=x[k]
$$

with initial conditions $y[-1]=y[-2]=0$ define a linear system with input $x[k]$ and output $y[k]$ ? If so, what is the order of this system? (Please briefly justify)

## 8. Getting Sparse With Linearity

Consider a novel sampling system that generates an output $\mathrm{f}_{\mathrm{c}}[\mathrm{k}]$ by sampling an input signal $\mathrm{u}[\mathrm{k}]$ to give the output via the following function:

$$
f_{c}[k]=\left\{\begin{array}{c}
u[k], \text { if } k \text { is odd } \\
0 \text { if } k \text { is even }
\end{array}\right.
$$

Is this system, $\mathrm{f}_{\mathrm{c}}[\mathrm{k}]$, linear and time invariant? (Please briefly justify)

## 9. Shattering Past Nyquist?

A crystal glass has a resonant frequency of 1100 Hz . A soprano sings this note exactly. If the note (treat it as a pure tone or sine wave) is amplified and transmitted using a digital amplifier that samples at 2000 Hz , will the glass shatter on the other side (assume arbitrarily high amplifier power)? (Please briefly justify)

## 10. Easy as ABC

Design a bandpass filter for tuning into TV content on Australian PAL B analog TV Channel 2. The QAM center frequency for this channel is $\mathbf{6 6 . 5} \mathbf{~ M H z}$. The channel width is 7 MHz (so $\pm \mathbf{3 . 5 ~ M H z}$ from the QAM center) ${ }^{1}$. The highest frequency in the tuning range $\left(f_{h}\right)$ is $\mathbf{2 5 7} \mathbf{~ M H z}$. The filter should have minimum transmission ( $\leq-20 \mathrm{~dB}$ ) at the neighbouring channel's QAM center frequencies ( 59.5 MHz and 73.5 MHz respectively) ${ }^{2}$.
a) What is the frequency range of the video signal and audio signal?
b) What type of filter should we use?
c) What order does this filter need to be?
d) What is the sampling rate needed for the circuit?
e) Please determine the transfer function and design this filter for these specifications.
f) Please sketch the frequency response of this filter.

[^0]
## Section 3: Digital Control

Please Record Answers in the Answer Book

## 11. Feedforward Block Diagram System Models

Please specify the transfer function $\left(T=\frac{y}{x}\right)$ for the following system.
[Hint: Please carefully note the forward direction of the arrows and the location of the sum element. This is not the "most common" feedback control block diagram]


## 12. Digital Stability

The transfer function of a sampled system is:

$$
T(z)=\frac{1}{z^{2}+(K-4) z+0.8}
$$

Please specify the range of K so that the system is stable.

## 13. Dynamic State-Space

Consider the system described by the following differential equations:

$$
\begin{gathered}
\dot{x_{1}}(t)=a_{1} x_{1}(t)+b_{1} u(t) \\
\dot{x_{2}}(t)=a_{2} x_{2}(t)+b_{2} u(t) \\
y(t)=x_{1}(t)+x_{2}(t)
\end{gathered}
$$

a) Please write this system in the standard state-space matrix form, that is, for

$$
\begin{aligned}
\dot{x}(t) & =\boldsymbol{A} x(t)+\boldsymbol{B} u(t) \\
y(t) & =\boldsymbol{C} x(t)+\boldsymbol{D} u(t)
\end{aligned}
$$

Determine the matrices $\mathbf{A}, \mathbf{B}, \mathbf{C}$, and $\mathbf{D}$ in terms of the constant parameters $a_{1}, a_{2}, b_{1}$, and $b_{2}$.
b) From this, please determine the system transfer function $\mathrm{H}(\mathrm{s})$ relating the output $\mathbf{Y}(\mathbf{s})$ to the input $\mathbf{U}(\mathbf{s})$.
(hint: $\left.H(s)=\frac{Y(s)}{U(s)}\right)$

## 14. Steer-by-Wire

A steer-by-wire system is proposed in which a DC motor regulates the hydraulic flow of a power steering system ${ }^{3}$. It has the following continuous time plant

$$
P(s)=\frac{1}{s(s+1)}
$$

The system is connected to a digital controller $\mathrm{D}(\mathrm{z})$ by a ZOH process ${ }^{4}$ having a period of $\mathbf{T}=\mathbf{0 . 1} \mathbf{s e c}$.

a) Determine G(z)
[hint: For this part you may leave it in terms of the $\mathbf{z}$-Transform, $\mathbf{Z}\{\boldsymbol{\bullet}\}$ (i.e. $\mathrm{G}(\mathrm{z})=\mathrm{Z}\{\mathrm{G}(\mathrm{s})\})$ )]
b) Sketch the impulse response of $\mathrm{G}(\mathrm{z})$
c) For a simple, proportional compensator, $\mathbf{D}(\mathbf{z})=\mathbf{K}$, please sketch the Root locus for this system.

[^1]
## 15. Lofty Controls!

Dr Shilling has a new disposable, biodegradable, stealth flying machine ${ }^{5}$. However, this system, especially when disturbed by the wind, is open-loop unstable.

The professor consulted Prof Tjohi, who advises that the system needs a controller ${ }^{6}$. He suggests a microprocessor with sampling time of $\mathbf{T}=\mathbf{0 . 0 3} \mathbf{s e c}$. With this in mind, Jeeves, the professor's assistant, performed system identification on the system. The spectra of the plant, of the disturbance, and of the measurement noise ${ }^{7}$ are shown in the figure below. The plant has one unstable pole at $\boldsymbol{\pi}=\mathbf{1}$. The reference for the control is $\boldsymbol{u}(\boldsymbol{t})=\mathbf{0}$.

a) Draw the block diagram of a generic, complete discrete-time control system, including interfaces, filters, and all relevant signals.
b) Can you do controller emulation in the case at hand?
(Please briefly justify)
c) Is an anti-aliasing filter necessary?
(Please briefly justify)
d) Based on these sections, Assess the stability of the discrete-time entire system. Will a simple, proportional controller be sufficient to regain stability?
END OF EXAMINATION — Thank you ©

[^2]
# ELEC 3004 / 7312: Signals Systems \& Controls Final Exam - 2013 

Table 1: Commonly used Formulae
The Laplace Transform

$$
F(s)=\int_{0}^{\infty} f(t) e^{-s t} d t
$$

The $\mathcal{Z}$ Transform

$$
F(z)=\sum_{n=0}^{\infty} f[n] z^{-n}
$$

IIR Filter Pre-warp

$$
\omega_{a}=\frac{2}{\Delta t} \tan \left(\frac{\omega_{d} \Delta t}{2}\right)
$$

Bi-linear Transform

$$
s=\frac{2\left(1-z^{-1}\right)}{\Delta t\left(1+z^{-1}\right)}
$$

FIR Filter Coefficients

$$
c_{n}=\frac{\Delta t}{\pi} \int_{0}^{\pi / \Delta t} H_{d}(\omega) \cos (n \omega \Delta t) d \omega
$$

Table 2: Comparison of Fourier representations.

\[

\]

Non-periodic Discrete-Time Fourier Transform

$$
X\left(e^{j \omega}\right)=\sum_{n=-\infty}^{\infty} x[n] e^{-j \omega n}
$$

$$
x[n]=\frac{1}{2 \pi} \int_{-\pi}^{\pi} X\left(e^{j \omega}\right) e^{j \omega n} d \omega
$$

## Fourier Transform

$$
X(j \omega)=\int_{-\infty}^{\infty} x(t) e^{-j \omega t} d t
$$

$$
x(t)=\frac{1}{2 \pi} \int_{-\infty}^{\infty} X(j \omega) e^{j \omega t} d \omega
$$

Continuous

Freq.
Domain

## ELEC 3004 / 7312: Signals Systems \& Controls <br> Final Exam - 2013

Table 3: Selected Fourier, Laplace and $z$-transform pairs.

| Signal | $\longleftrightarrow$ | Transform | ROC |
| :---: | :---: | :---: | :---: |
| $\tilde{x}[n]=\sum_{p=-\infty}^{\infty} \delta[n-p N]$ | $\stackrel{\text { DFT }}{\longleftrightarrow}$ | $\tilde{X}[k]=\frac{1}{N}$ |  |
| $x[n]=\delta[n]$ | $\stackrel{\text { DTFT }}{\longleftrightarrow}$ | $X\left(e^{j \omega}\right)=1$ |  |
| $\tilde{x}(t)=\sum_{p=-\infty}^{\infty} \delta(t-p T)$ | $\stackrel{\text { FS }}{\leftrightarrows}$ | $X[k]=\frac{1}{T}$ |  |
| $\delta_{T}[t]=\sum_{p=-\infty}^{\infty} \delta(t-p T)$ | $\stackrel{F T}{\rightleftarrows}$ | $X(j \omega)=\frac{2 \pi}{T} \sum_{k=-\infty}^{\infty} \delta\left(\omega-k \omega_{0}\right)$ |  |
| $\cos \left(\omega_{0} t\right)$ | $\stackrel{F T}{\rightleftarrows}$ | $X(j \omega)=\pi \delta\left(\omega-\omega_{0}\right)+\pi \delta\left(\omega+\omega_{0}\right)$ |  |
| $\sin \left(\omega_{0} t\right)$ | $\stackrel{F T}{\stackrel{F T}{\longrightarrow}}$ | $X(j \omega)=j \pi \delta\left(\omega+\omega_{0}\right)-j \pi \delta\left(\omega-\omega_{0}\right)$ |  |
| $x(t)= \begin{cases}1 & \text { when }\|t\| \leqslant T_{0} \\ 0 & \text { otherwise }\end{cases}$ | $\stackrel{F T}{\rightleftarrows}$ | $X(j \omega)=\frac{2 \sin \left(\omega T_{0}\right)}{\omega}$ |  |
| $x(t)=\frac{1}{\pi t} \sin \left(\omega_{c} t\right)$ | $\stackrel{F T}{\stackrel{F T}{\rightleftarrows}}$ | $X(j \omega)= \begin{cases}1 & \text { when }\|\omega\| \leqslant\left\|\omega_{c}\right\| \\ 0 & \text { otherwise }\end{cases}$ |  |
| $x(t)=\delta(t)$ | $\stackrel{\text { FT }}{\leftrightarrows}$ | $X(j \omega)=1$ |  |
| $x(t)=\delta\left(t-t_{0}\right)$ | $\stackrel{F T}{\rightleftarrows}$ | $X(j \omega)=e^{-j \omega t_{0}}$ |  |
| $x(t)=u(t)$ | $\stackrel{F T}{\stackrel{ }{\rightleftarrows}}$ | $X(j \omega)=\pi \delta(w)+\frac{1}{j w}$ |  |
| $x[n]=\frac{\omega_{c}}{\pi} \operatorname{sinc} \omega_{c} n$ | $\stackrel{\text { DTFT }}{\stackrel{\text { DTS}}{ }}$ | $X\left(e^{j \omega}\right)= \begin{cases}1 & \text { when }\|\omega\|<\left\|\omega_{\mathrm{c}}\right\| \\ 0 & \text { otherwise }\end{cases}$ |  |
| $x(t)=\delta(t)$ | $\stackrel{\mathcal{L}}{\leftrightarrow}$ | $X(s)=1$ | all $s$ |
| (unit step) $x(t)=u(t)$ | $\stackrel{\text { L }}{\stackrel{\text { L }}{\leftrightarrows}}$ | $X(s)=\frac{1}{s}$ |  |
| (unit ramp) $x(t)=t$ | $\stackrel{\mathcal{L}}{\leftrightarrow}$ | $X(s)=\frac{1}{s^{2}}$ |  |
| $x(t)=\sin \left(s_{0} t\right)$ | $\stackrel{\mathcal{L}}{\leftrightarrow}$ | $X(s)=\frac{s_{0}}{\left(s^{2}+s_{0}^{2}\right)}$ |  |
| $x(t)=\cos \left(s_{0} t\right)$ | $\stackrel{\mathcal{L}}{\stackrel{\text { L }}{ }}$ | $X(s)=\frac{s}{\left(s^{2}+s_{0}^{2}\right)}$ |  |
| $x(t)=e^{s_{0} t} u(t)$ | $\stackrel{\mathcal{L}}{\stackrel{\text { L }}{\longrightarrow}}$ | $X(s)=\frac{1}{s-s_{0}}$ | $\mathfrak{R e}\{s\}>\mathfrak{R e}\left\{s_{0}\right\}$ |
| $x[n]=\delta[n]$ | $\stackrel{z}{\longleftrightarrow}$ | $X(z)=1$ | all $z$ |
| $x[n]=\delta[n-m]$ | $\stackrel{\text { r }}{\leftrightarrow}$ | $X(z)=z^{-m}$ |  |
| $x[n]=u[n]$ | $\stackrel{z}{\stackrel{ }{\square}}$ | $X(z)=\frac{z}{z-1}$ |  |
| $x[n]=z_{0}^{n} u[n]$ | $\stackrel{z}{\leftrightarrows}$ | $X(z)=\frac{1}{1-z_{0} z^{-1}}$ | $\|z\|>\left\|z_{0}\right\|$ |
| $x[n]=-z_{0}^{n} u[-n-1]$ | $\stackrel{z}{\leftrightarrows}$ | $X(z)=\frac{1}{1-z_{0} z^{-1}}$ | $\|z\|<\left\|z_{0}\right\|$ |
| $x[n]=a^{n} u[n]$ | $\stackrel{\sim}{\stackrel{3}{4}}$ | $X(z)=\frac{z}{z-a}$ | $\|z\|<\|a\|$ |

## ELEC 3004 / 7312: Signals Systems \& Controls <br> Final Exam - 2013

Table 4: Properties of the Discrete-time Fourier Transform.

| Property | Time domain | Frequency domain |
| :--- | :---: | :---: |
| Linearity | $a x_{1}[n]+b x_{2}[n]$ | $a X_{1}\left(e^{j \omega}\right)+b X_{2}\left(e^{j \omega}\right)$ |
| Differentiation (fre- | $n x[n]$ | $j \frac{d X\left(e^{j \omega}\right)}{d \omega}$ |
| quency) | $x\left[n-n_{0}\right]$ | $e^{-j \omega n_{0}} X\left(e^{j \omega}\right)$ |
| Time-shift | $e^{j \omega_{0} n} x[n]$ | $X\left(e^{j\left(\omega-\omega_{0}\right)}\right)$ |
| Frequency-shift | $x_{1}[n] * x_{2}[n]$ | $X_{1}\left(e^{j \omega}\right) X_{2}\left(e^{j \omega}\right)$ |
| Convolution | $x_{1}[n] x_{2}[n]$ | $\frac{1}{2 \pi} X_{1}\left(e^{j \omega}\right) \circledast X_{2}\left(e^{j \omega}\right)$ |
| Modulation | $x[-n]$ | $X\left(e^{-j \omega}\right)$ |
| Time-reversal | $x^{*}[n]$ | $X^{*}\left(e^{-j \omega}\right)$ |
| Conjugation | $\mathfrak{I m}\{x[n]\}=0$ | $X\left(e^{j \omega}\right)=X^{*}\left(e^{-j \omega}\right)$ |
| Symmetry (real) | $\mathfrak{R e}\{x[n]\}=0$ | $X\left(e^{j \omega}\right)=-X^{*}\left(e^{-j \omega}\right)$ |
| Symmetry (imag) | $\sum_{n=-\infty}^{\infty}\|x[n]\|^{2}=\frac{1}{2 \pi} \int_{-\pi}^{\pi}\left\|X\left(e^{j \omega}\right)\right\|^{2} d \omega$ |  |
| Parseval |  |  |

Table 5: Properties of the Fourier series.

| Property | Time domain | Frequency domain |
| :--- | :---: | :---: |
| Linearity | $a \tilde{x}_{1}(t)+b \tilde{x}_{2}(t)$ | $a X_{1}[k]+b X_{2}[k]$ |
| Differentiation | $\frac{d \tilde{x}(t)}{d t}$ | $\frac{j 2 \pi k}{T} X[k]$ |
| (time) | $\tilde{x}\left(t-t_{0}\right)$ | $e^{-j 2 \pi k t_{0} / T} X[k]$ |
| Time-shift | $e^{j 2 \pi k_{0} t / T} \tilde{x}(t)$ | $X\left[k-k_{0}\right]$ |
| Frequency-shift | $\tilde{x}_{1}(t) \circledast \tilde{x}_{2}(t)$ | $T X_{1}[k] X_{2}[k]$ |
| Convolution | $\tilde{x}_{1}(t) \tilde{x}_{2}(t)$ | $X_{1}[k] * X_{2}[k]$ |
| Modulation | $\tilde{x}(-t)$ | $X[-k]$ |
| Time-reversal | $\tilde{x}^{*}(t)$ | $X^{*}[-k]$ |
| Conjugation | $\mathfrak{I m}\{\tilde{x}(t)\}=0$ | $X[k]=X^{*}[-k]$ |
| Symmetry (real) | $\mathfrak{R e}\{\tilde{x}(t)\}=0$ | $X[k]=-X^{*}[-k]$ |
| Symmetry (imag) | $\frac{1}{T} \int_{-T / 2}^{T / 2}\|\tilde{x}(t)\|^{2} d t=\sum_{k=-\infty}^{\infty}\|X[k]\|^{2}$ |  |
| Parseval |  |  |
|  |  |  |

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Table 6: Properties of the Fourier transform.

| Property | Time domain | Frequency domain |
| :--- | :---: | :---: |
| Linearity | $a \tilde{x}_{1}(t)+b \tilde{x}_{2}(t)$ | $a X_{1}(j \omega)+b X_{2}(j \omega)$ |
| Duality | $X(j t)$ | $2 \pi x(-\omega)$ |
| Differentiation | $\frac{d x(t)}{d t}$ | $j \omega X(j \omega)$ |
| Integration | $\int_{-\infty} x(\tau) d \tau$ | $\frac{1}{j \omega} X(j \omega)+\pi X(j 0) \delta(\omega)$ |
| Time-shift | $x\left(t-t_{0}\right)$ | $e^{-j \omega t_{0}} X(j \omega)$ |
| Frequency-shift | $e^{j \omega_{0} t} x(t)$ | $X\left(j\left(\omega-\omega_{0}\right)\right)$ |
| Convolution | $x_{1}(t) * x_{2}(t)$ | $X_{1}(j \omega) X_{2}(j \omega)$ |
| Modulation | $x_{1}(t) x_{2}(t)$ | $\frac{1}{2 \pi} X_{1}(j \omega) * X_{2}(j \omega)$ |
| Time-reversal | $x(-t)$ | $X(-j \omega)$ |
| Conjugation | $x^{*}(t)$ | $X^{*}(-j \omega)$ |
| Symmetry (real) | $\mathfrak{I m}\{x(t)\}=0$ | $X(j \omega)=X^{*}(-j \omega)$ |
| Symmetry (imag) | $\mathfrak{R e}\{x(t)\}=0$ | $X(j \omega)=-X^{*}(-j \omega)$ |
| Scaling | $x(a t)$ | $\frac{1}{\|a\|} X\left(\frac{j \omega}{a}\right)$ |
| Parseval | $\int_{-\infty}^{\infty}\|x(t)\|^{2} d t=\frac{1}{2 \pi} \int_{-\infty}^{\infty}\|X(j \omega)\|^{2} d \omega$ |  |

Table 7: Properties of the $z$-transform.

| Property | Time domain | $z$-domain | ROC |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Linearity | $a x_{1}[n]+b x_{2}[n]$ | $a X_{1}(z)+b X_{2}(z)$ | $\subseteq R_{x_{1}} \cap R_{x_{2}}$ |  |  |
| Time-shift | $x\left[n-n_{0}\right]$ | $z^{-n_{0}} X(z)$ | $R_{x}^{\dagger}$ |  |  |
| Scaling in $z$ | $z_{0}^{n} x[n]$ | $X\left(z / z_{0}\right)$ | $\left\|z_{0}\right\| R_{x}$ |  |  |
| Differentiation in $z$ | $n x[n]$ | $-z \frac{d X(z)}{d z}$ | $R_{x}^{\dagger}$ |  |  |
| Time-reversal | $x[-n]$ | $X(1 / z)$ | $1 / R_{x}$ |  |  |
| Conjugation | $x^{*}[n]$ | $X^{*}\left(z^{*}\right)$ | $R_{x}$ |  |  |
| Symmetry (real) | $\mathfrak{I m}\{x[n]\}=0$ | $X(z)=X^{*}\left(z^{*}\right)$ |  |  |  |
| Symmetry (imag) | $\mathfrak{R e}\{X[n]\}=0$ | $X(z)=-X^{*}\left(z^{*}\right)$ |  |  |  |
| Convolution | $x_{1}[n] * x_{2}[n]$ | $X_{1}(z) X_{2}(z)$ |  |  |  |
| Initial value | $x[n]=0, n<0 \Rightarrow x[0]=\lim _{z \rightarrow \infty} X(z)$ |  |  |  | $\subseteq R_{x_{1}} \cap R_{x_{2}}$ |

${ }^{\dagger} z=0$ or $z=\infty$ may have been added or removed from the ROC.

## ELEC 3004 / 7312: Signals Systems \& Controls <br> Final Exam - 2013

Table 8: Commonly used window functions.

## Rectangular:

$$
w_{\text {rect }}[n]= \begin{cases}1 & \text { when } 0 \leqslant n \leqslant M \\ 0 & \text { otherwise }\end{cases}
$$



## Bartlett (triangular):

$$
w_{\text {bart }}[n]= \begin{cases}2 n / M & \text { when } 0 \leqslant n \leqslant M / 2 \\ 2-2 n / M & \text { when } M / 2 \leqslant n \leqslant M \\ 0 & \text { otherwise }\end{cases}
$$



## Hanning:

$$
w_{\text {hann }}[n]= \begin{cases}\frac{1}{2}-\frac{1}{2} \cos (2 \pi n / M) & \text { when } 0 \leqslant n \leqslant M \\ 0 & \text { otherwise }\end{cases}
$$



## Hamming:

$$
w_{\text {hamm }}[n]= \begin{cases}0.54-0.46 \cos (2 \pi n / M) & \text { when } 0 \leqslant n \leqslant M \\ 0 & \text { otherwise }\end{cases}
$$



## Blackman:

$$
w_{\text {black }}[n]= \begin{cases}0.42-0.5 \cos (2 \pi n / M) & \text { when } 0 \leqslant n \leqslant M \\ +0.08 \cos (4 \pi n / M) & \text { otherwise }\end{cases}
$$



| Type of Window | Peak Side-Lobe Amplitude <br> (Relative; dB ) | Approximate Width <br> of Main Lobe | Peak Approximation Error, <br> $20 \log _{10} \delta(\mathrm{~dB})$ |
| :--- | :---: | :---: | :---: |
| Rectangular | -13 | $4 \pi /(M+1)$ | -21 |
| Bartlett | -25 | $8 \pi / M$ | -25 |
| Hanning | -31 | $8 \pi / M$ | -44 |
| Hamming | -41 | $8 \pi / M$ | -53 |
| Blackman | -57 | $12 \pi / M$ | -74 |




[^0]:    ${ }^{1}$ Analog television is broadcast with two carrier frequencies: one for video and one for audio. In the case of ABC TV, the vision carrier (for the QAM video) is at $\mathbf{6 4 . 2 5} \mathbf{~ M H z}$ and the audio carrier (for the FM audio) is at 69.75 MHz . A diagram showing the carrier frequencies within a PAL channel's 7 MHz of bandwidth is below:
    
    ${ }^{2}$ Technically, Channel 3 has a QAM center of 88.5 MHz as it is in VHF Band II, whereas Channel 2 is in VHF Band I. Please design for the given specification as this is generalizable to other 7 MHz wide channels.

[^1]:    ${ }^{3}$ Such systems are commercially available (often in very high-end vehicles) and should not be confused with all electric steer-by-wire systems (e.g. Nissan's Q50).
    ${ }^{4}$ Zero Order Hold. Recall that a ZOH is modelled by $G_{Z O H}=\frac{1-e^{-s T}}{s}$

[^2]:    ${ }^{5}$ Specifications and a prototype are in the appendix for your reference (p.15).
    ${ }^{6}$ In this way, it can be like the plane in "Paperman" (Pixar's Oscar-winning short film about lovely paper airplanes)
    ${ }^{7}$ This may be considered as zero mean, white "Gaussian" noise. (FYI, \$10 IMUs are not exactly "tactical grade.")

